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# Versatile and active THz wave polarization modulators using metamaterial/graphene resonators

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Active modification of the polarization state is a key feature for the next-generation of wireless communications, sensing, and imaging in the THz band. The polarization modulation performance of an integrated metamaterial/graphene device is investigated *via* a modified THz time domain spectroscopic system. Graphene's Fermi level is modified through electrostatic gating, thus modifying the device's overall optical response. Active tuning of ellipticity by > 0.3 is reported at the resonant frequency of 0.80 THz. The optical activity of transmitted THz radiations is continuously modified by > 21.5° at 0.71 THz. By carefully selecting the transmitted frequency with the relative angle between the incoming linear polarization and the device's symmetry axis, active circular dichroism and optical activity are almost independently exploited. Finally, this all-electronically tuneable versatile polarization device can be used in all applications requiring an ultrafast modulation such as polarization spectroscopy, imaging, and THz wireless generation.

#### KEYWORDS

terahertz, metamaterials, graphene, wireless communications, integrated modulators

# **1** Introduction

Recent research on optoelectronic modulators working in the terahertz (THz) band, ranging between 0.1-10 THz, has experienced an exponential growth due to its massive potential for applications, especially in the fields of wireless communications, spectroscopy, image sensing (Peiponen et al., 2013; Xu W. et al., 2017b; Zhang et al., 2021), and quantum electronics (Xu L. et al., 2017a; Liang et al., 2017; Wei et al., 2018; Fang et al., 2019; Mezzapesa et al., 2019; Almond et al., 2020; Jeannin et al., 2020; Wen et al., 2021). Amongst many approaches, only a few selected ones seem to provide flexibility, efficiency, and reconfiguration speed required by the disruptive technologies driven by the nextgeneration wireless communication scenarios. All-electronic approaches have represented a benchmark in the sub-THz range with remarkable performance reached by CMOS technology at 300 GHz recently (Venkatesh et al., 2020; Fujishima, 2021). Optoelectronic techniques, however, offer a higher level of miniaturization and efficiency above 500 GHz. Wireless communications beyond 5G are being deployed for mid- and near-field applications for ground communications, due to atmospheric absorption, on the promise of wide unallocated bandwidth and ultrafast communication (100 Gb-1 TB/s). An ultrafast communication platform is also needed for high-resolution imaging and sensing

for most of the applications which depict the future of digital society including the digital twin world, digital fabrications, augmented reality, or holograms. All of these hungry data-rate applications have motivated research into compact and integrated THz optoelectronic devices. We are here reporting an ultrafast versatile polarization modulator based on the interplay between graphene and metamaterials.

Metamaterials are artificial subwavelength resonant elements capable to provide an electromagnetic response beyond the material of composition. This approach has proved to be particularly efficient for achieving a continuous tuning of the polarization state of THz radiation, especially when combined with active materials such as phase change materials (Ma et al., 2020; Shabanpour, 2020; Ivanov et al., 2021), semiconductors (Pitchappa et al., 2019), graphene red (Kindness et al., 2019; 2020; Zheng et al., 2020; Masyukov et al., 2020; Zaman et al., 2022a; Zaman et al., 2022b), or in MEMS arrangement metasurfaces (Cong et al., 2019; Xu et al., 2021). Fermi-energy levels of a graphene monolayer can be altered either chemically or by electrostatic gating (Shafraniuk, 2015). MMs/ graphese polarization modulator was extensively investigated using gated double layers of graphene sheet reporting up to 95% of polarization conversion efficiency (Zhang et al., 2020). Ion-gel gating technique was deployed to allow chemical doping of graphene Fermi-energy which is significantly larger than electrostatic doping (Li et al., 2022), but it is not compatible with high all-electronic reconfiguration speed (>GHz). The interplay between single unit to collective states using 2DEG loaded metamaterials in a nested array arrangement has been adopted here as reported in (Zhang et al., 2015; Zhao et al., 2019), but using graphene as an active material. Recently, this modulator was tested all-electronically reporting a reconfiguration speed of 3 GHz, only limited by the available instrumentation (Zaman et al., 2022a). The same device was also optically pumped in an optical pump/THz probe experimental arrangement demonstrating reconfiguration speed's upper limit associated with the graphene's relaxation lifetime <2 ps as reported in (Zaman et al., 2022b) within a good agreement with acquainted literature on pristine graphene (Jnawali et al., 2013; Winnerl et al., 2013; Shi et al., 2014). In this paper, we begin with an overview of the device's design and fabrication. The following section presents the experimental setup and essential measurements. Then, the modulator is rotated by different angles in order to introduce cross-polarized E-fields to investigate the dynamic tuning of polarization plane rotation (OA) and circular dichroism (CD).

## 2 Design and fabrication

This complex design which has been described in detail in (Zaman et al., 2022a) is reminiscent of the nested architecture proposed by (Zhang et al., 2015; Zhao et al., 2019) using 2DEG as an active material. A double gate architecture has been used to ensure robust control of graphene's Fermi energy as well as a low operating bias voltage. The polarization mechanism is more similar to a tuneable metallic grid polarizer where the E-field polarized along its wires is rejected, rather than based on an engineered chiral response (Kindness et al., 2020) or EIT analogy (Kindness et al., 2019). The conductivity of graphene is high during the "on" state, and therefore the component of the E-field perpendicular to the

SR's orientation (i.e. y axis) becomes stronger and is transmitted. During the "off" state, however, the E-field is enhanced at resonance exhibiting a transmission of the pronounced dip as the graphene conductivity reaches its Dirac point (minimum conductivity).

The gated split resonators (gated/SRs) are fabricated after chemical vapor deposition (CVD) grown graphene transfer on a  $SiO_2/Si$  substrate (300 nm/500  $\mu$ m) (Burton et al., 2019). The Si substrate is slightly p-doped to allow back-gating. Graphene is then patterned into arrays of rectangles with  $16 \times 14 \,\mu\text{m}^2$  area size via lithographic masking followed by oxygen plasma etching (RF power = 50 W, 5 s). The gated SRs are fabricated by optical lithography followed by Ti/Au thermal evaporation (10 nm/150 nm) and liftoff shunting the graphene areas as shown in Figure 1A. Both the SRs and graphene areas are then encapsulated by Al<sub>2</sub>O<sub>3</sub> (150 nm) for protection and electrical isolation (Degl'Innocenti et al., 2017; Alexander-Webber et al., 2016). The top-gate is also formed by Ti/ Au on top of the Al<sub>2</sub>O<sub>3</sub> layer using electron beam lithography (E-beam) and positioned at the center of the SR's capacitive gap spacing as plotted in Figure 1A. The top gate's width shrinks to  $1.5 \,\mu m$ when passing through the center of the SRs' 7.5  $\mu$ m gap distance. The final arrangement of the SRs is realized as a combination of 20  $\times$ 22 resonators arranged in series and parallel configurations as illustrated in Figure 1B forming a total array dimension of 1.2  $\times$ 1.3 mm<sup>2</sup>. An optical microscope and scanning electron microscope (SEM) pictures of the fabricated array are shown in Figures 1C, D, respectively.

A single unite-cell's working principles are simulated using the RF module of COMSOL Multiphysics<sup>®</sup> software. A Drude model was used to simulate graphene conductivity as well as the metallic elements. When exciting the unite-cell with an x-polarized E-field (along the SR's axis), the E-field normalized is concentrated in the capacitive gap spacing during the "on" and "off" states at the 0.80 THz resonant frequency as plotted in Figures 2A, B, respectively. More details on simulation and fabrication are previously reported in (Zaman et al., 2022a).

# 3 Results and discussions

## 3.1 Preliminary measurements

To fully describe the polarization modulation, amplitudes and phases of the cross-polarization E-fields are separately acquired. Modulation depth (MD) of amplitudes or phases is a key factor to determine the quality performance of such a modulator. Generally, MD is defined as the normalized maximal excursion in amplitude (A) under an external stimulus as follows:

$$MD = A_{max} - A_{min} \tag{1}$$

Where A<sub>max</sub> and A<sub>min</sub> represent the maximum and minimum values.

### 3.1.1 Experimental setup

The device is inserted in a THz time-domain spectroscopy (THz-TDS) setup from Menlo Systems (model Tera K15) in transmission configuration with two grid polarizers, from Nearspec, positioned before and after the sample as illustrated in Figure 3. The THz emitter is always kept at the horizontal polarization state (i.e. along the x' axis) throughout the entire measurements. The first polarizer (PL) is rotated



#### FIGURE 1

(A) A unite-cell schematic picture showing its dimensions. (B) Top-view schematic picture of a complete gated SRs array. (C) Optical microscope and (D) SEM pictures of the fabricated SRs device.

by  $\Phi_{\rm PL} = 0^{\circ}$  with respect to the y' axis, i.e. vertical grids and full transmission, to select only the linear horizontal incident light. After passing through a pinhole (1.1 mm diameter), the device is mounted on a rotational moving stage which can be rotated by  $\theta_{SR} = 360^{\circ}$  with respect to the horizontal (x') axis allowing to excite both symmetry axes of the device (named x and y in Figure 3). A component of the incident E-field is parallel to the SR's plane of incident (E<sub>x</sub>), while the other is perpendicular to the SR's plane of incident (E<sub>v</sub>). The transmitted E-fields are then independently selected by rotating the analyzer's (AZ's) grids by an angle  $\Phi_{\rm AZ}$  with respect to the vertical axis, i.e. the y' axis.  $\Phi_{AZ}$  is rotated at different angles in accordance with the SRs' orientations ( $\theta_{SR}$ ). Lastly, transmitted waves through the AZ are detected by a THz receiver that is always set to the horizontal polarization state along the x' axis. During post-processing, the projection of E-fields on the receiver is taken into account by dividing the detected waves by sin/cos ( $\Phi_{AZ}$ ) based on the AZ's orientation.

#### 3.1.2 Optoelectronic response

The device is electrically biased by connecting the graphene's areas through the SRs' elements ( $V_{GND}$ ), whereas the back-gate is connected to the positive terminal of a DC power supply from a Kethely model 2450 source meter unit (SMU). These sets of measurements are acquired by using the back-gate electrical configuration since it is more robust than the top-gate and allows a larger biasing range without risking to incur any shortages. Topgating instead readily accessible and requires lower voltage range, but it is more susceptible to shortage mostly for wide biasing ranges. Therefore, it is faster and Compatible with fast data transmission applications. The device is driven with gate voltages  $(V_{BG})$  varying between -160 V and +160 V to alter the graphene conductivity around the Dirac point while measuring the gate leakage current (I<sub>BG</sub>). This range of driving voltages and Dirac point are comparable with other metamaterial devices previously reported in (Kindness et al., 2019; Kindness et al., 2020) where the 3 dB cut-off frequency



#### FIGURE 2

Simulations of a single unit-cell with an excitation of x-polarized (along the SR's axis)  $E_{norm}$ -fields at Y = +8  $\mu$ m (from the center), 0.8 THz resonant frequency, and graphene conductivity of (A) 0.2 mS "off" state and (B) 1.6 mS "on" state.



Schematic view of the THz time domain setup (THz-TDS) where the THz emitter and detector are horizontally polarized along the x' axis.  $\theta_{SR}$  and  $\phi$  are rotational angles with respect to x' and y' axes, respectively. L: lenses, PL: polarizer, PH: pinhole (Iris), V<sub>GND</sub>: ground connection that is always in contact with the graphene patches through the source and drain pads, V<sub>BG</sub>: top- or back-gates terminal, and AZ: analyzer.

reaches up to few MHz. Here, this device's architecture was tested all-electronically demonstrating a reconfiguration speed of >3 GHz, only limited by available electronics as previously presented in (Zaman et al., 2022a). During post-processing, the acquired temporal THz pulses are filtered either with a 30 ps unity rectangular window centered on the first pulse's peak or with a full (100 ps) unity rectangular window to consider all transmission and reflection E-fields arising from multiple reflections at the air/ sample boundaries (Fabry-Pérot resonances) as illustrated in Figure 4A. Single pulse transmission analysis provides all together comparison with the simulations and yields a direct evidence of the resonance supported by the SRs. By considering all the Fabry-Pérot resonances, it is possible to infer the device's behavior under a THz continuous wave source. Pulses passing through a 1.2  $\times$  1.2  $\mu$ m<sup>2</sup> uniform graphene patch fabricated on-chip without any SRs metal features are used for normalization, i.e. E<sub>ref</sub>. Unwanted absorption for frequencies above 1 THz clearly appears in the spectral amplitudes of  $E_{ref.}$ ,  $E_x$ , and  $E_y$  as shown in Figure 4B. Upon filtering temporal pulses, the acquired E-fields are normalized by referencing their spectral amplitudes to  $E_{ref.}$ 's amplitude, as shown in Figure 5A. At the same time, the extracted spectral phases are normalized by subtracting the spectral phase of  $E_{ref.}$ , as plotted in Figure 5B. Separate  $E_{ref.}$  waveforms were acquired each time the device was rotated while orienting both the PL and AZ to vertical grids (full transmission) position. A component of the incident E-field is parallel to the SR's plane of incident ( $E_x$ ), while the other is perpendicular to the SR's plane of incident ( $E_y$ ).

Graphene conductivity is dynamically modified by electrostatic gating, and therefore absorption of the incoming radiations at resonance is modified. Figure 6 reports the AM and PM modulation depths calculated for different device angles ( $\theta_{SR}$ ), from 5° to 75°. The MD was extracted for each  $\theta_{SR}$  angels from the



#### FIGURE 4

(A) Temporal THz E-fields normalized to the maximum value of the filtered first pulse. (B) Spectral amplitudes of the first transmitted temporal pulse at various back-gate voltages normalized with respect to the  $E_{ref.}$ 's maximum value when rotating the device by  $\theta_{SR}$  = 30° (from the x' axis) and analyzer by  $\Phi_{AZ} = -30^{\circ}$  and  $+60^{\circ}$  (from the y' axis). E<sub>ref.</sub> is the spectra of the first temporal pulse passing through a 1.2 x 1.2  $\mu$ m<sup>2</sup> uniform graphene patch fabricated on-chip without any SRs metal features and used for referencing.



#### FIGURE 5

Normalized spectral amplitudes (A) and relative phases (B) considering only the first temporal pulse at different  $V_{BG}$  voltages when  $\theta_{SR} = 30^{\circ}$  and  $\Phi_{A7} = -30^{\circ}$  and  $+60^{\circ}$ .



TABLE 1 Maximum MDs without considering multiple reflections.

Type of MD	E-field	$ heta_{ m SR}$ from the x' axis	Frequency (THz)	Continuous tuning (unit)
AM	Ex	5°	0.74	> 5.5 dB
	Ey	75°	0.62 & 0.63	> 3.75 dB
РМ	Ex	5°	0.68	> 18°
	Ey	75°	0.80	> 22.5°
Δη	//	5°	0.72	> 0.16 (ratio)
ΔΨ	//	5°	0.68	> 12°

TABLE 2 Maximum MDs when computing all the temporal pulses.

Type of MD	E-field	$ heta_{ m SR}$ from the x' axis	Frequency (THz)	Continuous tuning (unit)
AM	E <sub>x</sub>	5°	0.75	> 7.5 dB
	Ey	75°	0.61	>6 dB
PM	E <sub>x</sub>	45°	0.70	> 25°
	Ey	30°	0.60	> 10°
		5°	0.71	> 0.3 (ratio)
Δη	II	30°	0.70	> 0.16 (ratio)
		45°	0.70	> 0.21 (ratio)
		60°	0.62	> 0.15 (ratio)
		75°	0.62	> 0.11 (ratio)
		5°	0.71	> 21.5°
ΔΨ	II	30°	0.74	> 10°
		45°	0.70	> 12°
		60°	0.70	> 15°
		75°	0.70	> 9°

experimental data as shown in Figure 5 taking into consideration only the first temporal pulse. The MDs of E<sub>v</sub> polarization gradually shift towards smaller frequencies in order to match a dipole resonance along the orthogonal direction (the y axis). When focusing on 0.74 THz, Ex polarized waves encounter a sharp decrease in their spectral amplitude MDs when rotating the SRs by 75° with an average of ~5 dB as shown in Figure 6A. At the same frequency, orthogonal waves (Ey) encounter a sharp reduction in their MDs values as expected when exciting the SRs with orthogonal polarization. Although rotating the SRs' by an angle introduces different interactions with incident THz radiations, other factors should be taken into account; e.g. principally power attenuation. It comes with the drawback of excessive power losses. A summary of several MDs achieved considering only the first temporal pulse is reported in Table 1. When taking into account the entire temporal waveform during post-processing, Ex polarized lights have an enhanced spectral amplitude MD of >7.5 dB at 0.75 THz in correspondence with a device rotational angle ( $\theta_{SR}$ ) of 5°. Moreover, the E<sub>y</sub> polarized radiations have a spectral amplitude MD that exceeds 6 dB at 0.61 THz when  $\theta_{SR} = 75^{\circ}$  as summarized in Table 2 for considerations of the entire temporal waveforms.

Active changing of graphene conductivity also changes the phase of the supported resonant mode. By selecting only the first temporal pulse,  $E_x$  polarization reports a continuous change of ~ 18.5° in the MD of spectral phase at 0.68 THz when  $\theta_{SR} = 5^{\circ}$ . These results are also summarized in Table 1. At 0.80 THz,  $E_y$  polarization reaches its peak of MD with ~ 22.5° of continuous phase tuning when the SR is rotated by 75°. When focusing on 0.64 THz as presented in Figure 6B,  $E_x$  polarized waves have an average spectral phase MD of ~ 15° regardless of the SRs rotational angle. At the same frequency,  $E_y$  polarized spectral phases are continuously tuned by > 17° when  $\theta_{SR} = 75^{\circ}$ . When calculating all temporal pulses,  $E_x$  polarized waves have a continuous spectral phase tuning of > 25° when  $\theta_{SR} = 45^{\circ}$  at 0.70 THz. Additionally,  $E_y$  polarization has a spectral phase MD that reaches > 10° when  $\theta_{SR} = 30^{\circ}$  at 0.60 THz as summarized in Table 2.

## 3.2 Polarization modulation

These asymmetries in the  $E_{\mathrm{x/y}}$  amplitude and phase, which vary with the device rotational angle and incident frequency, can be



exploited into an active polarization device that highlights circular dichroism (CD) or optical activity (OA) depending on the user's selected configuration. The physical principle resembles the standard electro-optic modulator arrangement with crossed polarizers in the visible light as in (Yariv, 1989) or ultraviolet (Degl'Innocenti et al., 2007) range, but without the need for long crystals which would be impractical at these wavelengths. Other active metamaterial architectures demonstrated a similar mechanism by combining phase change materials (VO<sub>2</sub>) with metamaterial arrays (Ivanov et al., 2021). Whilst this approach is effective in yielding large modulation of polarization states, it can not match the ultrafast speed demonstrated by graphene-based modulators.

## 3.2.1 Theoretical description

The theoretical frame from (Wang et al., 2018; Ji et al., 2021; Lin et al., 2021) was used to better investigate and describe the performance of this device when operated as a polarization modulator. Alternative more comprehensive theoretical frames can be used to model these results, e.g. using the Poincare' sphere (Cai et al., 2021). However, for the case of flat metasurfaces with a well-defined polarization input state and wave-vector perpendicular

direction as in this case, a commonly used modelling based on Jones matrices is commonly adopted. The incoming linearly polarized light is projected into two perpendicular components E<sub>x</sub> and E<sub>v</sub> along the two symmetry axes of the device by rotating the sample as shown in Figure 3. These two E-field components experience a different complex refractive index. Electrostatic gating the graphene conductivity is modifying the complex refractive indices, hence causing different interactions for the cross-polarized transmitted E-field waves. Changes in the real part of the refractive index is producing a continuous tuning in the rotation of polarization plane (OA), while changes in the imaginary part of the refractive index is causing dynamic manipulations in ellipticity ratio of the elliptically polarized transmitted radiations (CD). The transmitted linearly polarized coefficients selected by the analyzer are converted into circular ones by following Jones formalism as follows (Wang et al., 2018; Ji et al., 2019; 2021; Fan et al., 2021; Lin et al., 2021):

$$\begin{pmatrix} E_{RCP}(\omega) \\ E_{LCP}(\omega) \end{pmatrix} = \frac{1}{\sqrt{2}} \begin{pmatrix} 1 & i \\ 1 & -i \end{pmatrix} \begin{pmatrix} E_x(\omega) \\ E_y(\omega) \end{pmatrix}$$
$$= \frac{1}{\sqrt{2}} \begin{pmatrix} 1 & i \\ 1 & -i \end{pmatrix} \begin{pmatrix} |E_x(\omega)|e^{i\angle E_x(\omega)} \\ |E_y(\omega)|e^{i\angle E_y(\omega)} \end{pmatrix}$$
(2)



Where  $E_x$  and  $E_y$  complex components are the transmitted vectors projected either along or orthogonal to the SR's axis (x or y), respectively. Both detected fields are normalized with respect to the  $E_{ref.}$  pulses with the graphene sheet reference rotated by the same rotational angle as the SRs' orientation. Both linear and circular components are used to describe either the OA ( $\Psi$ ) or CD ( $\eta$ ) as follows (Wang et al., 2018; Ji et al., 2019; Fan et al., 2021; Lin et al., 2021):

$$\Psi(\omega) = \frac{1}{2} \cdot \tan^{-1} \left\{ \tan \left[ 2 \cdot \frac{|E_x(\omega)|}{|E_y(\omega)|} \right] \cdot \cos \left[ \angle E_x(\omega) - \angle E_y(\omega) \right] \right\} \quad (3)$$

$$\eta(\omega) = \frac{|E_{RCP}(\omega)| - |E_{LCP}(\omega)|}{|E_{RCP}(\omega)| + |E_{LCP}(\omega)|}$$
(4)

Where  $\Psi(\omega)$  and  $\eta(\omega)$  units are in degrees and dimensionless, respectively.  $E_{RCP}$  and  $E_{LCP}$  complex values, in Eq. 4, are calculated using Eq. 2. The linear scale of  $\eta$  indicates the ratio between the elliptical major and minor axes, hence complete linear or perfect circular polarization states correspond to 0 or ±1, respectively. Independent control of the OA and CD is a key element for achieving more degrees of freedom for polarization modulators, even though it is difficult to achieve the two effects independently. The detected linear transmission coefficients are also used to retrieve the state of polarization ellipses. The quadratic equation in Cartesian components of the ellipses is described as follows (Ji et al., 2019; Fan et al., 2021):



$$\frac{E_{x'}^2}{|E_x|^2} - 2 \cdot \frac{E_{x'}E_{y'}}{|E_x||E_y|} \cdot \cos(\angle E_x - \angle E_y) + \frac{E_{y'}^2}{|E_y|^2} = \sin^2(\angle E_x - \angle E_y)$$
(5)

Where  $E_x$  and  $E_y$  are the major and minor axes of an elliptically polarized wave and represent the transmitted E-fields projected along the modulator's axes. Eq. 5 is solved in bipolar coordinates with their major and minor vectors' magnitudes normalized to the maximum value of the major vector prior plotting the polarization curves.

## 3.2.2 Single pulse processing

For each applied voltage, both cross-polarization waves transmitted from the device are consecutively acquired by rotating the analyzer with the correct  $\Phi_{AZ}$  angle based on the SR's orientations. During post-processing, the first temporal pulse is considered throughout this section's data analysis as plotted in Figure 4A. Continuous rotation of  $\Psi$  by ~ 6.5° is observed at 0.75 THz when rotating the device by  $\theta_{SR} = 30^{\circ}$  and for a voltage sweep between -120 V and +120 V as shown in Figure 7A. The maximum difference between the amplitudes of  $E_{RCP}$  and  $E_{LCP}$  (not shown here) is resulting in maximum modifications of  $\eta$  at 0.72 THz from ~0.33 to ~0.45 as illustrated in Figure 7B. The maximum modulation depth of OA ( $\Delta\Psi$ ) is a 12° of continuous tuning at 0.68 THz when  $\theta_{SR}$  is 5° as summarized in Table 1. As shown in Figure 7C, the peaks of  $\Delta\Psi$  decrease when exciting the SRs with any other angle far from the 0°.  $\Delta\Psi$  peaks start degrading sharply for all  $\theta_{SR}$  above 75°. Similarly, the depth

of ellipticity changes ( $\Delta \eta$ ) is maximized with 0.16 when the SRs are rotated by 5° at 0.72 THz as summarized in Table 1. Dynamics of  $\Delta \eta$ remain almost steady for all SRs' angles ranging from 30° to 60° with an average  $\Delta \eta$  of 0.11 at different frequencies as plotted in Figure 7D. Active changes of  $\Delta \eta$  are sharply decreased when rotating the SRs by 75°. Another interesting observation is that the peaks of dynamic tuning of  $\Delta \Psi$  and  $\Delta \eta$  keep shifting gradually towards smaller frequencies when increasing the SRs' angle from 30° to 60°. Polarization ellipses, shown in Figures 8A-H, further highlight the independent control of OA and CD. When rotating the device by 45°, for example, the maximum  $\Delta \eta$  of 0.11 occurs at 0.65 THz with a minimal change in the  $\Delta \Psi$  by only 1.3°. On the other hand, maximum tuning of  $\Psi$  by 6.4° takes place at 0.73 THz with a minimal  $\Delta \eta$  of 0.04. The same observation is reported for other rotational angles of  $\theta_{\rm SR}$  at different frequencies. Depending on the sample rotational angle and incoming frequency, it is possible with this approach to selectively enhance either OA or CD. This is of a great importance with polarization spectroscopy (Choi et al., 2019), polarization imaging (Watanabe, 2018), or THz applications in the pharmaceutical (Markl et al., 2018) or biomedical fields, e.g. (Son, 2020). It is worth mentioning that  $\eta$  is reversing its sign at 0.80 THz when rotating the device by  $\theta_{SR} = 60^{\circ}$  (not shown here). This ultrafast switching of the light handedness finds application in spintronics or characterization of topological materials (Bader and Parkin, 2010; Plank and Ganichev, 2018; Liu et al., 2020; Liu et al., 2021; Papaioannou and Beigang, 2021).

#### 3.2.3 All pulses processing

The inclusion of all temporal pulses during post-processing, however, offers a further opportunity to enhance the modulation of the polarization state at the same frequencies. Dynamic changes of  $\Psi$  and  $\eta$  exceed 21.5° and 0.3, respectively, at 0.71 THz and  $\theta_{SR} = 5^{\circ}$  as presented by the polarization ellipses in Figure 9A for various back-gate voltages. Moreover, decoupling of OA and CD is observed when rotating the SRs by any other angle besides  $\theta_{SR} = 5^{\circ}$  as shown in Figures 9B–K and reported in Table 2. When  $\theta_{SR} = 45^{\circ}$ , dynamics of  $\Delta\eta$  are also maximized to > 0.21 at 0.70 THz while continuous tuning of  $\Psi$  is exceeding > 12° as shown in Figures 9B, C; respectively.

## 4 Conclusion

External integrated optoelectronic polarization modulators based on the interplay between graphene and metallic metamaterial arrays have been investigated by terahertz timedomain spectroscopy for applications such as GHz-speed communication, spectroscopy, and imaging. By electrostatic gating the graphene/metamaterials split resonators, polarization modulation was reported with dynamic conversions from linear to elliptical polarization states. When processing only the first temporal pulse, the amplitude extinction ratio was demonstrated achieving > 5.5 dB at 0.74 THz for the  $E_x$  polarized waves. The

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Alexander-Webber, J. A., Sagade, A. A., Aria, A. I., Veldhoven, Z. A. V., Braeuninger-Weimer, P., Wang, R., et al. (2016). Encapsulation of graphene transistors and vertical device integration by interface engineering with atomic layer deposited oxide. 2D Mater 4, 011008. doi:10.1088/2053-1583/4/1/011008 spectral phase could be actively tuned by >22° at 0.63 THz for the E<sub>y</sub> polarization. The modulation depths of  $\eta$  were dynamically changed by >0.16 in ellipticity ratio at 0.72 THz while  $\Psi$  were continuously rotated by >12° at 0.68 THz. When processing all temporal pulses, the amplitude modulation depths were enhanced to exceed 7.5 dB at the resonant frequency for the E<sub>x</sub> polarization. The spectral phase was dynamically manipulated by >25° at 0.70 THz for the E<sub>x</sub> polarization. Almost independent control of CD and OA was demonstrated achieving  $\Delta \eta = >0.3$  and  $\Delta \Psi = >21.5°$ , respectively, at 0.71 THz. These remarkable performances along with >GHz switching speed all-electronically represent a step forward toward various applications such as in next-generation wireless communication, spectroscopy, and imaging.

## Data availability statement

Publicly available datasets were analyzed in this study. This data can be found here: Lancaster University's repository, https://doi.org/10.17635/lancaster/researchdata/562.

## Author contributions

AZ, NA, JG, HB, DR, OB, JA-W, SH, and TM did part of fabrication. AZ, YL, and RD'I did the measurements. AZ did post-processing and wrote the article together with contribution from all coauthors. RD'I and AZ conceived the idea.

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# Conflict of interest

The authors declare that the research was conducted in the absence of any commercial or financial relationships that could be construed as a potential conflict of interest.

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