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**Biofunctional silk kirigami with engineered properties**

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## Abstract

The fabrication of multifunctional materials that interface with living environments is a problem of great interest. A variety of structural design concepts have been integrated with functional materials to form biodevices and surfaces for health monitoring. In particular, approaches based on kirigami-inspired cuts can engineer flexibility in materials through the creation of patterned defects. Here, the fabrication of a biodegradable and biofunctional “silk kirigami” material is demonstrated. Mechanically flexible, free-standing, optically transparent, large-area biomaterial sheets with precisely defined and computationally designed microscale cuts can be formed using a single-step photolithographic process. Using modeling techniques, it is shown how cuts can generate remarkable “self-shielding” leading to engineered elastic behavior and deformation. As composites with conducting polymers, flexible, intrinsically electroactive sheets can be formed. Importantly, the silk-kirigami sheets are biocompatible, can serve as substrates for cell culture, and be proteolytically resorbed. The unique properties of silk kirigami suggest a host of applications as transient, “green”, functional biointerfaces, and flexible bioelectronics.

**Keywords:** silk fibroin, kirigami, micropatterning, conducting polymer, flexible, biodegradable

## 1. Introduction

Producing flexible, thin, mechanically robust and compliant interfaces which perform in dynamic environments is an ongoing challenge.<sup>1-2</sup> Such multifunctionality can establish adaptive interfaces with the body.<sup>3</sup> From human-machine interfaces and soft robotics, to implantable devices and engineered tissues for regenerative medicine, material design and fabrication strategies have focused on capturing the mechanical compliance and biomimetic sensing of skin.<sup>4-6</sup> Various architectures have been proposed to impart functional conformability with biological tissues including meshes, cracks, prestressing, buckling, and serpentine designs.<sup>7-8</sup> Integrating biocompatibility and biodegradation can vastly expand the scope of synthetic “skins” for applications in biohybrid systems, soft matter electronics,<sup>9</sup> prosthetics,<sup>10</sup> wound healing, neural interfaces, and health monitoring *in situ*.<sup>11-12</sup> Across length scales, micropatterned and microstructured materials may be used for cell co-cultures and spatial control.<sup>13-15</sup> Recently, approaches building on principles borrowed from the Japanese paper arts such as origami and kirigami, have shown great promise.<sup>16</sup> Origami refers to folding (“*ori-*”), whereas kirigami involves cutting (“*kiri-*”) of paper (“*-gami*”). Complex and functional objects using combinations of cutting, bending, and/or folding of diverse materials have been shown artistically and scientifically.<sup>17</sup>

Of interest is the use of kirigami-inspired cuts to transform materials towards multifunctional biointerfaces. While designed to enhance elasticity for traditionally stiff materials, kirigami architectures can transform intrinsically flexible and soft materials in interesting ways. For instance, mechanical properties at scales smaller than the cuts would not change, whereas effective properties at scales larger than the cuts would.<sup>18</sup> Substrates can be imbued with deformability

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3 beyond the strain limits of pristine materials, allowing for multifunctionality e.g. stretchability,  
4 conformability to complex interfaces, conductivity, fault tolerance, biocompatibility, and  
5 reconfigurability. Out-of-plane deformations can enable reversible geometry changes,  
6 transforming between planar 2D and 3D.<sup>8, 17, 19</sup> Using computational tools, it is possible to predict  
7 and thereby precisely engineer, the operative behaviors under mechanical stresses.  
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12 Previously, kirigami cuts have been accomplished using subtractive methods including microscale  
13 laser cutting,<sup>20</sup> optical lithography,<sup>21</sup> etching (e.g. plasma, masked ion),<sup>22</sup> and macroscopic cutting  
14 (e.g. x-acto knives).<sup>23</sup> In addition to the traditionally used paper, elastomers  
15 (polydimethylsiloxane), metal foils, plastics (polyimide, polyethylene terephthalate, polyester  
16 films), and graphene-silk composite are among materials reported.<sup>16-17</sup> (Table S1 in the supporting  
17 information provides several recent examples). To impart conductivity, metal electrodes (Au, Ag,  
18 Pt, Al), indium tin oxide, carbon nanomaterials (nanotubes, graphene), conducting polymers, and  
19 2D layered materials such as MoS<sub>2</sub>, have been used.<sup>7, 21, 24-25</sup> A top-down, lithographic process was  
20 shown in a graphene oxide-polyvinyl alcohol nanocomposite with cuts formed using plasma  
21 etching through photoresist patterns deposited on the nanocomposite.<sup>22</sup> However, the use of fully  
22 biodegradable and biocompatible materials with kirigami strategies has not been shown.  
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41 For the first time, photolithographic fabrication of biofunctional, biodegradable silk kirigami via  
42 a facile, single step subtractive process is demonstrated. “Protein lithography” via photoreactive  
43 silk fibroin is utilized as a route to multiscale fabrication.<sup>26-27</sup> The biomaterial behaves as a  
44 negative-tone photoresist, crosslinking under UV irradiation. Whereas traditional kirigami uses  
45 cuts to form desired topologies, a photocurable material permits using photolithography to remove  
46 uncrosslinked material. This results in flexible, free-standing, optically transparent, macroscale  
47 sheets with precisely defined microscale cuts. Using finite element modeling and fracture  
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3 mechanics, a framework can be established to predict the stretching behavior of these films and  
4 their strength, as a function of different cut geometries. Cuts can bring about remarkable “self-  
5 shielding” leading to engineered elastic behavior. Silk-kirigami sheets are biocompatible, can  
6 serve as substrates for cell culture, and be proteolytically degraded. By doping with the conducting  
7 polymer polyaniline, intrinsically conducting silk kirigami films are demonstrated that are flexible,  
8 stretchable, and can be bent and twisted while retaining electrical properties. As mechanically-  
9 tunable cell scaffolds coupled with electrochemical properties, the use of bioinspired silk kirigami  
10 to form degradable and biocompatible, yet functional substrates facilitates advanced capabilities  
11 as engineered tissues and (bio)electronic interfaces.<sup>11, 28-29</sup>  
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## 27 **2. Results and Discussion**

### 28 *2.1. Fabrication of flexible silk fibroin kirigami*

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34 Kirigami-inspired cuts/patterns using degradable and biocompatible polymers can add a new  
35 dimension to their function. Silk proteins form a versatile class of bioresorbable biomaterials for  
36 drug delivery, nanostructured scaffolds,<sup>30</sup> and recently, implantable bioelectronics, photonics, and  
37 bio-integrated devices.<sup>31-32</sup> Here, microfabrication of flexible, optically transparent kirigami films  
38 is realized using a light-reactive silk protein with a rapid, scalable process.<sup>26, 33</sup> Material subtraction  
39 or cutting is photolithographically accomplished in a single step process. The solution of  
40 photocrosslinkable (silk) fibroin in hexafluoroisopropanol was crosslinked by exposure through a  
41 photomask, resulting in complex patterns (Figure 1). As a negative-tone photoresist-like material,  
42 uncrosslinked material is developed, and the resulting free-standing silk kirigami sheet easily  
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3 peeled off. The sheets formed are stable in a wide range of solvents, and can be stored in air or  
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5 water over several weeks without degradation.<sup>27,33</sup>  
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8 The cuts have a high structural fidelity and spatial resolution demonstrating the scalability and  
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10 accuracy of this photolithographic process to form micropatterns over large areas. SEM imaging  
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12 shows ordered patterns of various complexities over a large area (cm scale) of flexible fibroin sheet  
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14 (Figure 2b-f). They are optically transparent (Figure 2a), shown here with cuts – 50  $\mu\text{m}$  wide, 500  
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16  $\mu\text{m}$  long, enabling potential use in stretchable optics and transparent devices.<sup>34</sup> Cuts down to  $\sim 10$   
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18  $\mu\text{m}$  using benchtop lithography can be easily formed, with nanoscale patterns possible using  
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20 electron beam lithography.<sup>35</sup> The micro-cut kirigami films are mechanically robust and can be  
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22 held, rolled or bent into various conformations without any loss in their physico-chemical-  
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24 mechanical properties. Bending certain patterns such as branches, saddles, or chevrons result in  
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26 interesting and useful microscale openings and out-of-plane deformations (Figure 2), (Figure S1).  
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28 In an unanticipated result, it was observed that partial cuts, particularly at smaller feature sizes,  
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30 could be formed by reducing the time of crosslinking. This results in films that can have engineered  
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32 weakness along the partial cuts (Figure S2).  
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39 Films tens of  $\mu\text{m}$  thick are easily formed by controlling the amount of solution cast and the spin  
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41 coating speed (films reported here are formed with thickness of 20-25  $\mu\text{m}$ , confirmed by optical  
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43 and electron microscopy). While the dry films are flexible but not compliant, moist films can be  
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45 applied to, and readily conform to irregular surfaces (e.g. skin) (Figure 2g) without the need for  
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47 adhesives. In comparison, a pristine film of similar size and thickness is quickly delaminated on  
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49 bending the finger. The results show that moist silk kirigami films display enhanced adhesion to  
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51 skin similar to earlier reported laser-cut PDMS.<sup>36</sup> Human skin is known to be stretchable to 75%  
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53 strain, with surface strains  $\sim 55\%$  at the knees.<sup>37</sup> The introduction of deformability in silk kirigami  
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3 sheets, with fracture-resistant openings to accommodate stretch allows highly conformable  
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5 interfaces or attachment at interfaces.<sup>38</sup>  
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## 10 11 *2.2. Tensile testing and finite-element modeling*

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14 Kirigami-based structural designs can achieve dynamic shaping towards stretchability and  
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16 foldability.<sup>39</sup> Kirigami sheets possess a mechanical regime in which they are stretchable and soft  
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18 in comparison to pristine (uncut) sheets.<sup>40</sup> The mechanical properties are dramatically affected by  
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20 the presence of the cuts resulting in a desired large enhanced deformability but in undesired  
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22 weakening, as predicted by fracture mechanics. Tensile testing was conducted on thin silk kirigami  
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24 films with a simple, uniform slit geometry. Experimental values were obtained for two sets of cuts  
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26 – 100  $\mu\text{m}$  wide x 500  $\mu\text{m}$  and 100  $\mu\text{m}$  x 1000  $\mu\text{m}$  long, as well as a branched geometry – ‘Y’-  
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28 cuts). Measurements were taken at a strain rate of 0.1 mm/s. Consistent with prior reports, pristine  
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30 (uncut) silk films have a high breaking stress but fail at strains of  $\sim 7\%$  (Figure S3).<sup>41</sup> In contrast,  
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32 with a simple cut geometry, even completely dry silk kirigami films can be easily stretched to a  
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34 strain of  $\sim 40\%$  (Figure 3a – middle panel). The breaking strain recorded is typically below the  
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36 strain at which the films completely fail. Even though some of the cuts tear, the entire structure  
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38 does not come apart (Figure S4, S5). The stills from the tensile test with the point of failure (red-  
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40 arrow) under load are shown in Figure S4).  
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47 The stress-strain response were then modeled using the Finite Element Method (FEM) software  
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49 ABAQUS, which provides a high level of flexibility, reliability, and verifiability.<sup>19, 22, 36</sup> A  
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51 parametric script was used to define different mechanical, geometrical boundary conditions. Input  
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53 parameters used to perform a specific simulation varied geometry, material properties [Young’s  
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3 modulus  $E$ , Poisson ratio  $\nu$ , density values of silk fibroin were used], and loading conditions. The  
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5 mechanical constitutive model is elastoplastic with isotropic linear elasticity and linear hardening.  
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7 The simulation allows the introduction of a “defect” in correspondence with the middle point of  
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9 each cut which triggers the out-of-plane instability typically observed in kirigami structures. This  
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11 used preliminary buckling analysis and a nonlinear quasi-static analysis under uniaxial tension.  
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13 From Figure 3a, the excellent correlation and predictive ability of the simulations with the  
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15 experimentally observed tensile behavior is noted, even at high strain. The stress visualizations at  
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17 the crack tips are shown in Figure 4 for the slit geometry and the branched geometry under  
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19 increasing loads (2-6 MPa). Complete details and videos of the simulations are provided in the  
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21 Supporting Information. Using the predictive abilities of this FEM analysis, it is possible to *ab*  
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23 *initio* design kirigami geometries for various applications.  
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### 32 *2.3. Fracture mechanics and design of self-shielding cuts*

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35 A mathematical model was developed for the geometries tested to provide a framework for the  
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37 strength of the silk kirigami films. The model is based on diamond-shaped arrays of “cracks” which  
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39 are strikingly similar in geometry to the cut patterns.<sup>42-43</sup> Assumptions of linear elastic fracture  
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41 mechanics, derived from the method of continuous dislocation distributions were applied. Briefly,  
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43 considering the geometry shown in Figure 3 and 5, the kirigami shape factor  $Y$  depends on the  
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45 half-length of the cuts ( $a$ ) and the center-to-center horizontal ( $d$ ) and vertical separation ( $b$ )  
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47 between two consecutive cuts.  $Y$  accounts for the finiteness of the body with respect to the cut  
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49 length. For example, a relatively short cut could act as a single central cut in an infinite plane, for  
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51 which the shape factor is  $Y = 1$ . If the vertical spacing is large enough ( $b/2a \rightarrow \infty$ ), then the shape  
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53 factor may be approximated by a single row of collinear cuts (Figure 5b). Its general definition is:  
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$$Y = (1 - s) \quad (1)$$

where  $-\infty \leq s \leq 1$  is a calculated self-shielding factor dependent on the cut geometry (Table S2).<sup>43</sup>

It is postulated that the cut overlaps protect each other resulting in a self-shielding mechanism in the kirigami films. If the vertical spacing is small enough ( $b/2a \rightarrow 0$ ), this shielding mechanism occurs for overlapping rows of cuts (Figure 5a and 5c). Using these expressions, the critical strength  $\sigma^c$  of the various kirigami geometries and design self-shielding cuts can be estimated.

$$\sigma_c^\infty = \frac{K_{Ic}}{Y\sqrt{\pi a}} = \frac{K_{Ic}}{(1 - s(\frac{b}{2a} \frac{d}{2a}))\sqrt{\pi a}} \quad (2)$$

$K_{Ic}$  is the critical stress intensity factor, estimated using properties of silk fibroin. Films with longer cuts have a larger cut overlap, resulting in effective shielding. For a cut length of 500  $\mu\text{m}$ , the shape factor is  $Y_{500} = 0.65$ , while for 1000  $\mu\text{m}$  cuts, the shape factor is  $Y_{1000} = 0.3$ . The ratio between critical strengths is therefore theoretically estimated to be 1.5, which favorably compares to the experimental value of  $\sim 1.2$ . A small discrepancy occurs because the technique of continuous dislocation distributions does not account for out-of-plane instability and the plastic hardening observed both experimentally and in FEM simulations. However, these values offer a satisfactory comparison, confirming the design of self-shielding cuts in silk kirigami.

The behavior of patterns with branched cuts can similarly be estimated. The stress intensity factor  $K_{I_{br}}$  of a symmetric single branched cut in an infinite medium was estimated using the continuous dislocation distribution technique.<sup>42, 44</sup> In this system, the length of the inclined branch ( $c$ ) = length of the horizontal branch ( $a$ ) = 200  $\mu\text{m}$  and  $\theta$  (inclination of the branch) =  $60^\circ$ . It is assumed that the interactions for a diamond-shaped array of straight cuts also apply to a diamond-shaped array of branched cuts. For branched cuts, the vertical separation is  $b = 866 \mu\text{m}$ , and horizontal

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3 separation is  $d = 700 \mu\text{m}$ , corresponding to the condition of cut overlap. The shape factor is  $Y_{\text{br}} \approx$   
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5  $0.65 = Y_{500}$ . Therefore, the ratio of critical strength between the two kirigami with straight and  
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7 branched cuts is  $\sim 1.7$ , which only slightly overestimates the strength of the kirigami with branched  
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9 cuts (ratio  $\sim 1.4$ ). Coupled with FEM simulations, such mathematical formulations therefore allow  
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11 computationally design of self-shielding kirigami cuts with precisely engineered strength and  
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13 stretchability.  
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#### 20 21 *2.4. Evaluation of biocompatibility and degradation*

  
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23 Substrates capable of supporting cell growth and providing topographical and spatial cellular  
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25 control, can deliver insight into the dynamics of cell interactions, while providing for ordered cell-  
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27 sheets, and cell-based biosensors.<sup>45</sup> Flexible polymeric meshes<sup>46</sup> and ultrathin polymeric films  
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29 have been previously proposed as functional nanomembranes for directing cellular organization.<sup>12</sup>  
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31 Precise micro and nanoscale surface cuts on a mechanically robust, stretchable biomimetic  
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33 substrate provides fascinating opportunities to direct the behavior of cells, control cell  
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35 morphology, interface with tissue, and provide shape-programmability.<sup>47</sup> The biocompatibility and  
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37 non-cytotoxicity of the substrate biomaterial was earlier shown.<sup>27</sup> Cell viability was assessed using  
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39 an MTT assay (Figure S6) showing that the silk kirigami films are conducive to viability and  
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41 metabolic activity. To verify the potential for cell guidance on silk-kirigami, the mouse myoblast  
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43 cell line C2C12 cells were studied. The kirigami films are robust enough to withstand sterilization  
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45 procedures allowing for cell patterning (Figure 6). Two different conditions were explored to  
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47 promote cell attachment - preconditioning with expansion media, and coating with human  
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49 fibronectin. After 7 days of culture, the cell cytoskeleton and nuclei were stained with I-Fluor 488  
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51 and DAPI, respectively, and observed by confocal microscopy. Cells showed adherence to both  
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3 samples, but a higher and more homogeneous adhesion was observed on kirigami sheets  
4 preconditioned with expansion media (Figure 6b-d). This condition had the optimal proliferation  
5 rate and organization of the cells. Expectedly, the controls (TCP and uncut fibroin films) also  
6 showed good adhesion of cells (Figure S7). DAPI was completely absorbed by the films and used  
7 only to show the underlying organization of the cuts (blue films – Figure 6c).

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15 The topographical features of the kirigami design clearly align adhesion along the cuts, guiding  
16 the cells via surface morphology. Moreover, the imaging highlights cell alignment on the edges of  
17 the cuts, and the formation of cytoskeletal bridges linking the sides of the holes (Figure 6b). Similar  
18 bridging was observed for fibronectin coated films (Figure S8). Such flexible, stretchable cell  
19 culture sheets can therefore be used for fundamental studies of 3D tissue models, where the cuts  
20 can guide cells, and the underlying sheets eventually degrade over time. Cuts also provide the  
21 opportunity to form sheets with communication and mass transfer between sheets. Biodegradable,  
22 free standing, flexible cell sheets can potentially be stacked to generate 3D multilayered structures,  
23 with conformal contact at the bio-interface.<sup>48</sup> By dissolving a fluorescent molecule within the  
24 fibroin solution, fluorescent kirigami in a variety of designs (Figure 6a) can be formed. In these  
25 films, the uniform green fluorescence is derived from FITC-dextran (MW 4 kDa).

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41 An advantage in using silk kirigami in addition to its biocompatibility, is the ability of the materials  
42 to be controllably degraded in physiological environments. Proteolytic action results in  
43 degradation of the silk kirigami sheets leading to the complete loss of mass and structural integrity.  
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48 An enzymatic biodegradation experiment was conducted on silk kirigami films incubated in PBS  
49 solution with or without protease (control) at 37°C. Due to proteolytic biodegradation, a loss of  
50 weight was observed, and after 10 days, the films incubated in the enzyme broke down, whereas  
51 the control samples maintained their integrity and flexibility (Figure S9). This was consistent with  
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3 previous observations in which the biodegradability of fibroin based flexible devices can be tuned  
4 by controlling the degree of crosslinking and film thickness.<sup>26, 33, 49</sup> Stretchable devices and  
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6 biointerfaces with precisely engineered lifetimes can therefore be fabricated using the kirigami  
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8 films, which can be useful as flexible biomimetic cellular constructs for tissue regeneration, drug  
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10 delivery platforms, and biosensors.  
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### 18 *2.5. Conducting silk kirigami*

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21 While many soft materials are not potentially degradable or resorbable, conducting polymer  
22 composites with silk<sup>50-51</sup> and auxetic patches using chitosan,<sup>52</sup> have been used towards tissue-  
23 interfacing electronics, and e-textiles.<sup>10, 39, 53</sup> Graphene oxide biopaper was reported with high  
24 electrical conductivity.<sup>54</sup> It may be noted that this was primarily graphene oxide, with only 2-5%  
25 of silk fibroin to provide binding interactions. Silk-based bioelectronics have potential for  
26 advanced bio-applications, primarily as a bioresorbable substrate for ultrathin electronics.<sup>31</sup>  
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28 Multifunctional kirigami with intrinsic electrical conductivity is demonstrated by incorporating  
29 the conducting polymer polyaniline (PANI) to form fully organic electroactive sheets. PANI has  
30 a high temperature resistance, environmental stability, and excellent electrical conductivity.<sup>55</sup>  
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32 While PANI solubility is typically low in most solvents, it is soluble in the benign solvent formic  
33 acid which makes it suitable to form silk composites.<sup>33</sup> Initially, compositions were optimized for  
34 both electrochemical and mechanical properties. The presence of H-bonding between the benzene  
35 ring structures of the molecular backbone of PANI causes rigidity in the composite films making  
36 the films brittle at high concentrations.<sup>55</sup> High PANI concentrations impart a dark color to the  
37 films, making photolithography difficult (e.g. cuts < 100  $\mu\text{m}$  are not easily formed). 1% PEG as a  
38 plasticizer was used to improve the flexibility of the silk sheets at optimal PANI concentrations  
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3 (11% w/w), resulting in mechanically robust and flexible films (Figure 7a).  
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6 Conducting kirigami films were made in a similar manner, via UV crosslinking through a  
7 photomask followed by development. The electrical conductivity was probed by forming  
8 connecting pads at the ends (Figure S10). Initially, kirigami films were compared to pristine  
9 (uncut) films of similar size. For the sake of simplicity, the linear cut geometry was tested. The  
10 difference in conductivity (Figure 7b) indicates that the properties of the films are a function of  
11 the cut geometry. Excellent conductive behavior was observed ( $\mu\text{S}$  conductance levels and linear  
12 behavior over a voltage range of  $-0.5 - +0.5$  V). The films (slit width  $100\ \mu\text{m}$ , length  $500\ \mu\text{m}$ , gap  
13 spacing  $-500\ \mu\text{m}$  and gap width  $500\ \mu\text{m}$ ,  $25\ \mu\text{m}$  thick) retain their conductivity under stretch  
14 (Figure S11), although the conductance changes  $\sim 40\%$  under  $10\%$  linear strain. An underlying  
15 PDMS slab was used as a support to precisely control the angle of bend and twist (Figure 7c,  
16 Figure S12). A bend of  $50-55^\circ$  was performed in these experiments to simulate the bending at the  
17 knee.<sup>37</sup> The films themselves are stable and function independently of the support. A change in  
18 conductance from  $3.03\ \mu\text{S}$  to  $2.35\ \mu\text{S}$  ( $\sim 22\%$ ) was observed in the film on  $55^\circ$  bend. The  
19 conductance changes as a function of stretch and also bending, which indicates that the composites  
20 undergo conformational changes on mechanical deformation. However, the films remain  
21 conductive under twist and  $180^\circ$  bend (Figure 7d) Coupled with the deformability and  
22 stretchability shown, these intrinsically conducting silk kirigami films can therefore be designed  
23 for skin-like devices, with a better understanding of the electrochemical behavior linked to the  
24 dynamics of deformation.<sup>38</sup> As bioinspired and degradable platforms that can be formed in a green  
25 fashion, this platform can go a long way towards addressing sustainability in bioelectronics.<sup>56</sup>  
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### 3. Conclusions

In summary, the fabrication of multifunctional silk kirigami films using a facile photolithographic technique is demonstrated. The kirigami films themselves are simultaneously extremely stretchable and robust thanks to self-shielding cuts, and can be formed at various thicknesses ranging from thin (ca.  $\mu\text{m}$ ) to thick (10s of microns), as well as degradable. The cut geometries of these films can be easily engineered via light-assisted microfabrication, which permits the formation of complex, high resolution architectures at high throughput and scale. The computational FEM and theoretical fracture mechanics models guide and support the experimental findings, and provide insight into the modes of deformation and fracture including the presence of self-shielding cuts and influence of geometry. Critically, these silk kirigami films are biocompatible and display the ability to spatially direct cell growth along the cut geometry, while also being controllably biodegradable. It is also possible to modulate the electrochemical characteristics of the films by doping with the conducting polymer polyaniline. These results suggest that silk kirigami can provide exceptional bioinspired and biodegradable structures towards flexible and stretchable biodevices.

### 4. Experimental Section

#### *Fabrication of micropatterned kirigami films using photocrosslinkable fibroin*

Photocrosslinkable fibroin (referred to as fibroin protein photoresist or photofibroin) was prepared by the incorporation of photoreactive moieties to fibroin as reported earlier.<sup>26</sup> 7.5% (w/v) of photofibroin was dissolved in HFIP with 2.5% (w/v) photoinitiator (Irgacure 2959, BASF). The solution was drop cast on plain glass slides and air dried for 15 minutes to evaporate excess solvent.

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3 Samples were crosslinked using 365 nm UV (Lumen Dynamics OmniCure 1000) at 20 mW cm<sup>-2</sup>.  
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5 Uncrosslinked areas (cuts) were developed by soaking in 1M LiCl/DMSO. Free-standing films  
6  
7 were obtained by soaking developed films in de-ionized water to delaminate them from the glass  
8  
9 support. Films were washed in water and stored in air or water. To form conducting fibroin films,  
10  
11 polyaniline (PANI) emeraldine salt from p-toluenesulfonic acid (Alfa Aesar, Tewksbury, MA) (11  
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13 % w/w) and photofibroin were dissolved in formic acid. Similar fabrication steps were followed.  
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### 17 *Electrochemical Characterization*

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20 Linear sweep voltammetry (LSV) was used to characterize the electrochemical properties of the  
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22 silk-PANI kirigami films. The measurement was conducted by a Gamry Interface 1010E  
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24 Potentiostat (Gamry Instruments, Warminster, PA). The scanning range of applied potential was  
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26 from – 0.5 V to 0.5 V (over 1V) with a rate of 100 mV/s. The electrochemical data was analyzed  
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28 using Gamry Echem Analyst software. Electrical connections were testing by connecting to a DC  
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30 power source.  
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### 34 *Tensile tests*

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37 Kirigami samples fixed on a paper frame with a window of 0.5 cm side. The tensile test was  
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39 performed on an MTS 300 series tensile testing machine (MTS Systems Corporation, Eden Prairie,  
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41 MN) equipped with a 50 N load cell. Measurements were taken at a strain rate of 0.1 mm/s and  
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43 data was collected at a rate of 10 Hz. All other parameters are sample specific such as thickness,  
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45 width and length. Typically, films were 20-25 μm thick.  
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### 50 *Finite element modeling and simulation*

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53 The commercial software ABAQUS was used to compute the deformations of the kirigami films  
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55 for the three patterns in Figure 3a. The mesh is composed of 6-node triangular thin shell elements  
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3 (STRI65) near the tips to limit elements distortion upon cut opening, and 8-node quadrangular thin  
4 shells (S8R5) for the rest of the domain. A convergence analysis through mesh refinement was  
5 conducted to ensure mathematical accuracy. The final ratio between average mesh size (and the  
6 width of the films was 560) and the cut width was 4. An elastoplastic isotropic linear elastic  
7 constitutive model, with linear hardening was used. The material properties are Young Modulus  
8 248 MPa, Poisson ratio 0.3, yield stress 12.92 MPa, hardening coefficient 26.36 MPa. To stabilize  
9 the dynamic implicit simulations, artificial numerical damping is introduced (by setting the  
10 parameters  $\alpha = -0.41421$ ,  $\beta = 0.5$  and  $\gamma = 0.91421$  in the Hilber-Hughes-Taylor time integration).  
11 Quasi-static conditions are ensured by monitoring the kinetic energy.  
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#### 24 *Cell culture experiments*

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27 Mouse muscle myoblast cells (C2C12) were expanded in medium consisting in DMEM high  
28 glucose (Euroclone), 10% Fetal Bovine serum (Euroclone), 1% antibiotic/antimycotic  
29 (Euroclone), 1% L-glutamine (Euroclone), and 1% sodium Pyruvate (GIBCO). Cells were cultured  
30 in 75 cm<sup>2</sup> flask at 37°C and 5% CO<sub>2</sub> in humidified atmosphere and expanded until 70% confluence  
31 was reached. For this experiment the cell passage was 16. Samples were pretreated by two different  
32 methods - one group was preconditioned with complete expansion medium at 37°C for 30 minutes,  
33 the other was incubated with human fibronectin (Sigma Aldrich) for 1 hour at 37°C. As a control  
34 silk fibroin sheets without cuts were used and preconditioned with complete expansion medium  
35 and with human fibronectin, as kirigami films. All samples were sterilized with 70% ethanol for  
36 40 minutes and then washed twice with sterile PBS (Euroclone).  
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#### 51 *Morphological evaluation of adhered cells*

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54 Adhered cell morphology on kirigami sheets were studied by imagining by confocal microscopy  
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3 at day 7 after seeding using Nikon A1 Laser Microscope. Before confocal observations, samples  
4 were fixed with 4% PFA for 40 minutes, permeabilized with 0.2% Triton X-100 for 30 minutes.  
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6 The nuclei and the cell cytoskeleton were stained with DAPI (Sigma-Aldrich) and I-Fluor 488  
7  
8 (Abcam), respectively, per the manufacturers' instruction.  
9

### 10 11 12 13 *Proteolytic degradation in vitro*

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16 Silk fibroin films can be proteolytically degraded over time in the presence of enzymes. In the  
17 present work, the degradation of silk kirigami films in the presence of protease (Protease XIV from  
18 *Streptomyces griseus*,  $\geq 3.5$  U mg<sup>-1</sup>, Sigma Aldrich) was demonstrated. Films - 20  $\mu$ m thick with  
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20 100  $\mu$ m cuts (containing  $\sim 2.5$  mg fibroin) were incubated in 5 mL protease (1 U mg<sup>-1</sup> of protein)  
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22 at 37 °C and the degradation was studied over 2 weeks. Note that this protease concentration is  
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24  $\sim 3$ x the prior used concentrations, resulting in a comparatively rapid degradation.<sup>26, 33, 49</sup> Another  
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26 set of samples were incubated in PBS buffer under the same environment, which served as the  
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28 negative control. The enzyme solution was replaced every 3 days to maintain protease activity.  
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30 Samples from each set were taken out on different days, rinsed with DI water, and imaged under  
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32 a microscope to record their degradation over time.  
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### 43 **Supporting Information**

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45 Supporting information showing prior kirigami literature, additional images of the silk kirigami,  
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47 MTT assay, cellular spreading, mathematical modeling, simulations, tensile behavior, and  
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49 conductive silk kirigami are provided. Videos of the tensile simulations are shown.  
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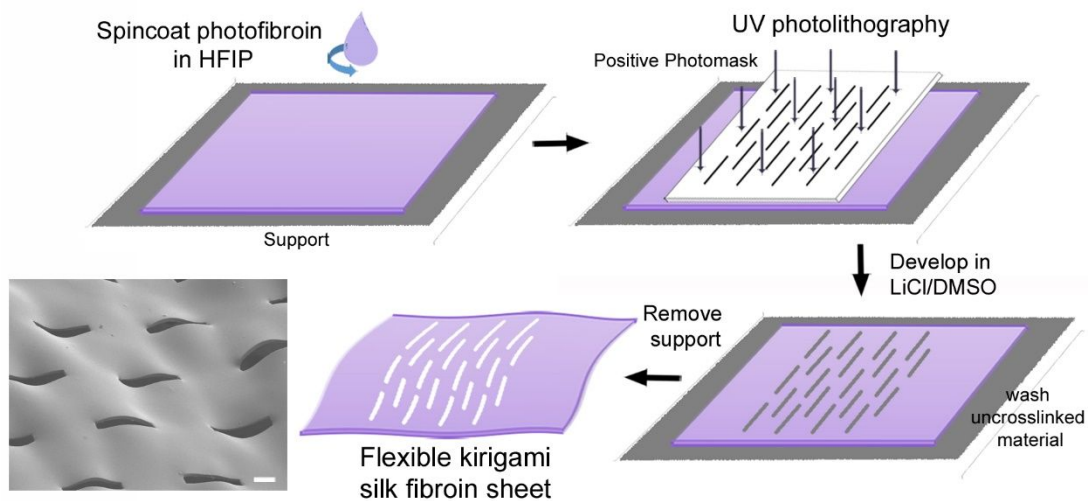
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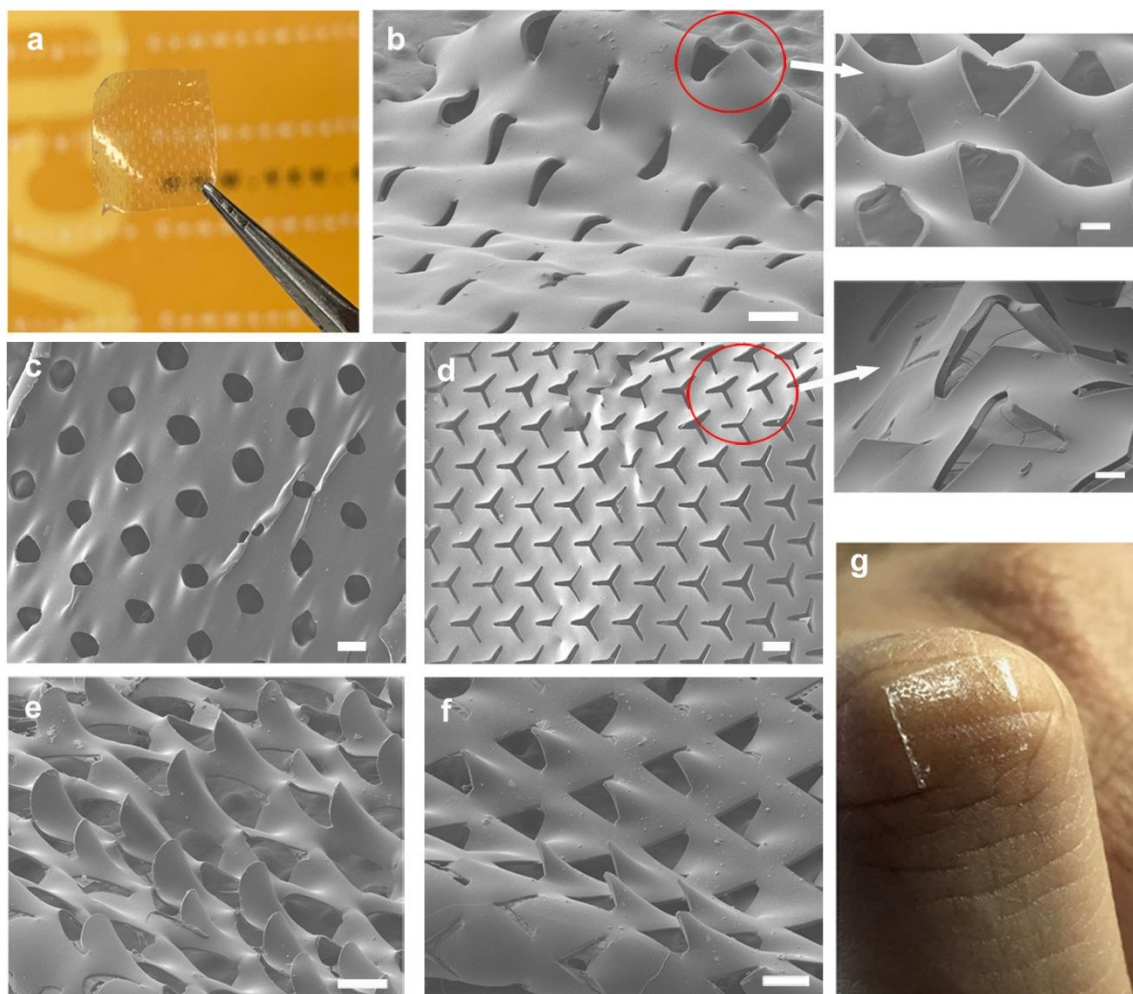
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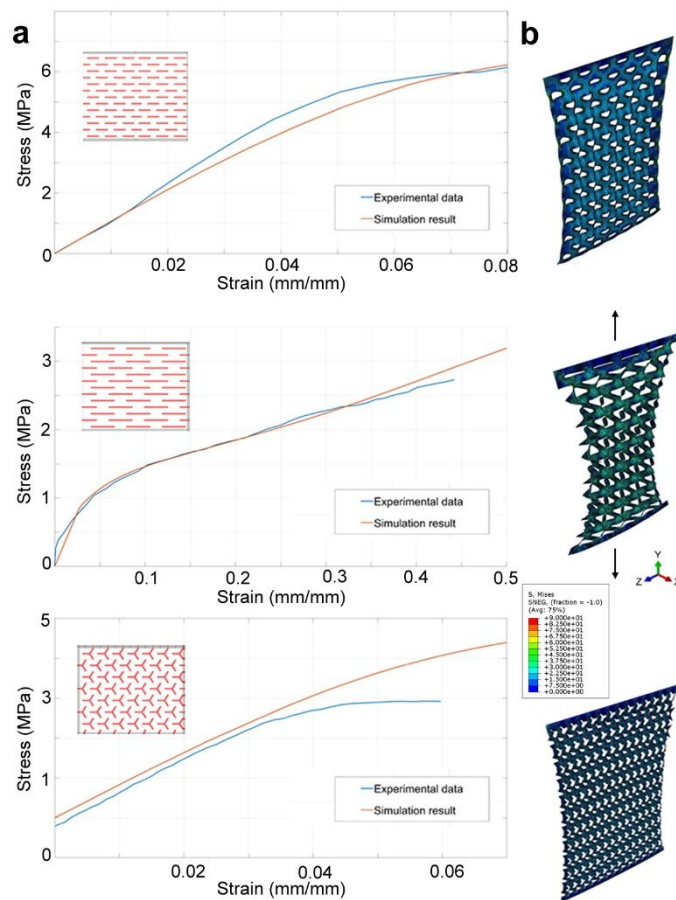




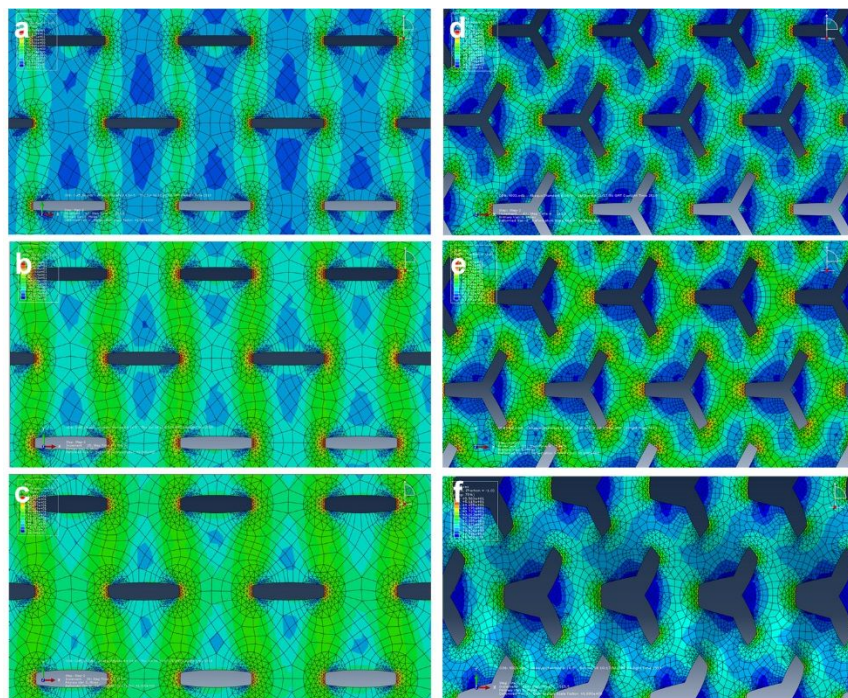
**Figure 1:** Schematic: Single step fabrication of kirigami cuts in silk fibroin films via photolithography.



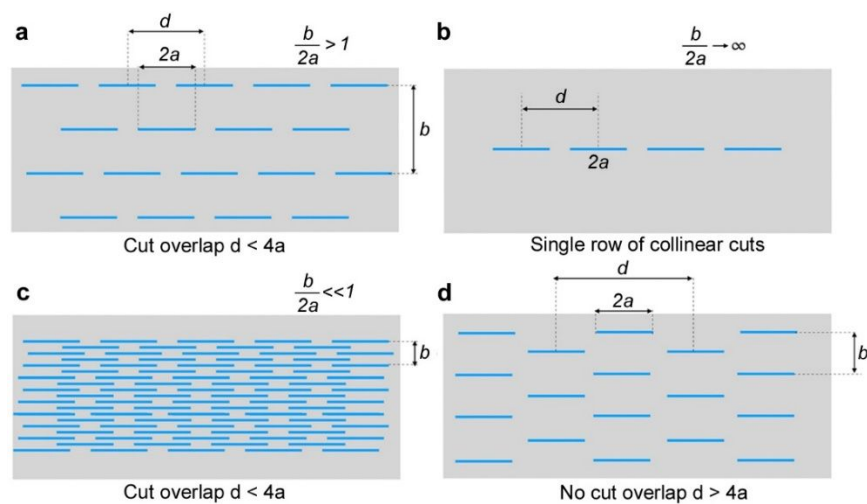
**Figure 2:** Imaging of silk kirigami **a.** Large scale silk kirigami films can be formed that are optically transparent (shown here are cuts 50  $\mu\text{m}$  wide x 500  $\mu\text{m}$  long). SEM images showing the diversity of geometries of cuts that can be formed using photolithography – **b.** linear cut geometry with 25  $\mu\text{m}$  cuts, **c.** cross cuts that can be stretched biaxially, **d.** branched ('Y'-cuts), **e.** saddles **f.** chevrons. The top right insets show the out of plane deformation of the cuts. **g.** adherence of film shown in (a) to skin. The film is moist in this case and remains on during finger flexure. Scale bar on all images = 100  $\mu\text{m}$ . Film thickness = 25  $\mu\text{m}$ .



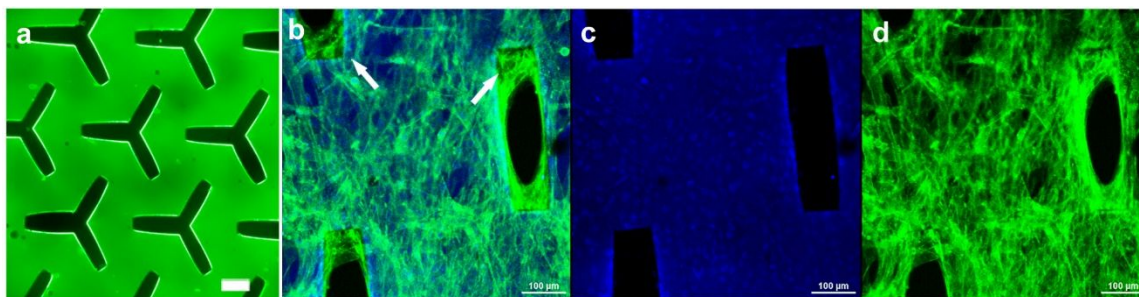
**Figure 3:** Mechanical behavior and simulations **a.** Stress-strain curves for different kirigami patterns: (top) shorter linear cuts (500  $\mu\text{m}$ ), (middle) longer linear cuts (1000  $\mu\text{m}$ ), and (bottom) branched cuts ('Y'-shapes) and their respective deformations – (red line: simulation result; blue line: experimental data). The contour plot reports the von Mises stress values. **b.** Visualization of the FEM modeling corresponding to the cuts shown. The scale bar shows increasing stress from blue to red.



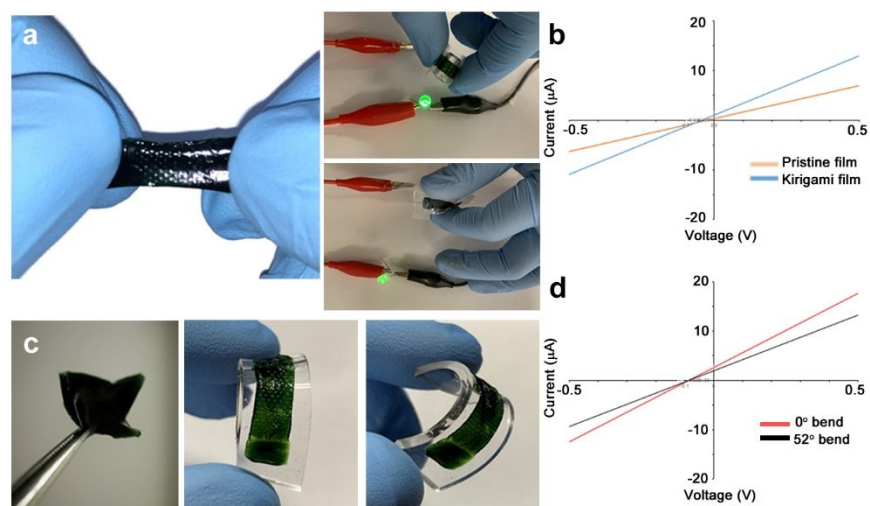
**Figure 4:** Visualization of the stress concentrations near the cut tips under increasing load conditions (top to bottom 2, 4 and 6 MPa) for a (a-c) slit geometry (500  $\mu\text{m}$  length) and (d-f) branched (Y-shaped) cut geometry with 200  $\mu\text{m}$  arm length.



**Figure 5:** Kirigami patterns as **(a, c, d)** diamond-shaped array of cuts, and, **(b)** single row of collinear cuts.

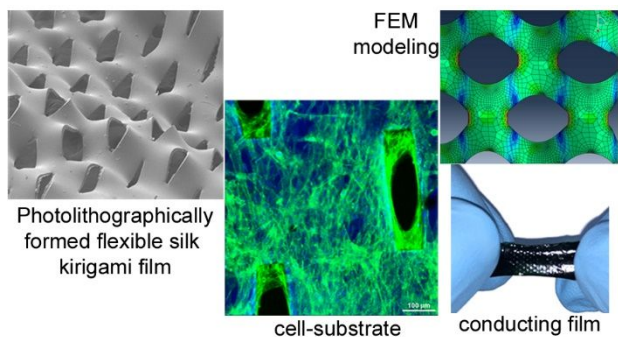


**Figure 6:** Functionality of silk kirigami **a.** Fibroin kirigami films can be loaded with fluorescent dyes (shown here – FITC-dextran MW 4 kDa). **b.** Adherence of C2C12 cells to the silk kirigami films 7 days after seeding. The arrows show the cytoskeletal bridges across the cuts. **c, d.** DAPI and actin staining.



**Figure 7. a.** Electrically conducting, mechanically robust kirigami sheets that can be bent and twisted. Films are conductive enough to illuminate an LED under both bending and twisting. **b.** comparison of electrical behavior between a pristine (uncut) film and a kirigami film of similar size. **c.** Sheets can be folded and unfolded. A PDMS slab was used to provide support for measurement under bending. **d.** Comparison of behavior in relaxed ( $0^\circ$ ) and bent ( $52^\circ$ ) condition. Film thickness =  $25 \mu\text{m}$ .

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Photolithographically formed flexible silk kirigami film

FEM modeling

cell-substrate

conducting film